



Approval body for construction products and types of construction

Bautechnisches Prüfamt

An institution established by the Federal and Laender Governments



European Technical Assessment

ETA-11/0190 of 23 July 2018

English translation prepared by DIBt - Original version in German language

General Part

Technical Assessment Body issuing the European Technical Assessment:	Deutsches Institut für Bautechnik
Trade name of the construction product	Würth self-tapping screws
Product family to which the construction product belongs	Self-tapping screws for use in timber constructions
Manufacturer	Adolf Würth GmbH & Co. KG Reinhold-Würth-Straße 12-17 74653 Künzelsau DEUTSCHLAND
Manufacturing plant	Werk 1, Werk 2, Werk 3, Werk 4, Werk 5, Werk 6, Werk 7, Werk 8, Werk 9, Werk 10, Werk 11, Werk 12, Werk 13, Werk 14, Werk 15, Werk 16, Werk 17, Werk 18, Werk 19, Werk 20
This European Technical Assessment contains	112 pages including 9 annexes which form an integral part of this assessment
This European Technical Assessment is issued in accordance with Regulation (EU) No 305/2011, on the basis of	EAD 130118-00-0603
This version replaces	ETA-11/0190 issued on 27 June 2013



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Specific part

1 Technical description of the product

Würth "ASSY", "Jamo", "Amo" and "WG Fix" screws are self-tapping screws made from special carbon or stainless steel. Screws made from carbon steel are hardened, except "ASSY-ISOTOP" screws. They are anti-friction coated and they have a corrosion protection according to Annex A.2.6. The outer thread diameter d is not less than 3.0 mm and not greater than 14.0 mm. The overall length of the screws is ranging from 13 mm to 2000 mm. Further dimensions are shown in Annex 9. The washers are made from carbon or stainless steel, aluminium or copper. The dimensions of the washers are given in Annex 9.

2 Specification of the intended use in accordance with the applicable European Assessment Document

The performances given in Section 3 are only valid if the screws are used in compliance with the specifications and conditions given in Annex 1 and 2.

The verifications and assessment methods on which this European Technical Assessment is based lead to the assumption of a working life of the screws of at least 50 years. The indications given on the working life cannot be interpreted as a guarantee given by the producer, but are to be regarded only as a means for choosing the right products in relation to the expected economically reasonable working life of the works.

3 Performance of the product and references to the methods used for its assessment

3.1 Mechanical resistance and stability (BWR 1)

Essential characteristic	Performance
Dimensions	See Annex 9
Characteristic yield moment	See Annex 2
Characteristic withdrawal parameter	See Annex 2
Characteristic head pull-through parameter	See Annex 2
Characteristic tensile strength	See Annex 2
Characteristic yield strength	See Annex 2
Characteristic torsional strength	See Annex 2
Insertion moment	See Annex 2
Spacing, end and edge distances of the screws and minimum thickness of the wood based material	See Annex 2
Slip modulus for mainly axially loaded screws	See Annex 2



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3.2 Safety in case of fire (BWR 2)

Essential characteristic	Performance
Reaction to fire	Class A1

3.3 Safety and accessibility in use (BWR 4)

Same as BWR 1

4 Assessment and verification of constancy of performance (AVCP) system applied, with reference to its legal base

In accordance with EAD No. 130118-00-0603 the applicable European legal act is: 97/176/EC. The system to be applied is: 3

5 Technical details necessary for the implementation of the AVCP system, as provided for in the applicable EAD

Technical details necessary for the implementation of the AVCP system are laid down in the control plan deposited with Deutsches Institut für Bautechnik.

Issued in Berlin on 23 July 2018 by Deutsches Institut für Bautechnik

BD Dipl.-Ing. Andreas Kummerow Head of Department *beglaubigt:* Dewitt



Annex 1 Specifications of intended use

A.1.1 Use of the Würth screws only for:

- Static and quasi-static loads

A.1.2 Base materials

The screws are used for connections in load bearing timber structures between wood-based members or between those members and steel members:

- Solid timber (softwood) according to EN 14081-1¹,
- Solid timber of beech, ash or oak according to EN 14081-1,
- Glued laminated timber (softwood) according to EN 14080²,
- Glued laminated timber made from beech, ash or oak according to European Technical Assessment or national provisions that apply at the installation site,
- Laminated veneer lumber LVL of softwood according to EN 14374³,
- FST according to ETA-14/0354,
- Glued solid timber (softwood) according to EN 14080 or national provisions that apply at the installation site,
- Cross-laminated timber (softwood) according to European Technical Assessment or national provisions that apply at the installation site,
- − Oriented Strand Board, OSB/3 and OSB/4 according to EN 300⁴ and EN 13986⁵ with $\rho_k \ge 550$ kg/m³,
- − Particleboard according to EN 312⁶ and EN 13986 with $ρ_k \ge 640$ kg/m³,
- Solid-wood panels according to EN 13353⁷ and EN 13986
- Gypsum plasterboards for load-bearing applications according to European Technical Assessment with $\rho \ge 650 \text{ kg/m}^3$,
- fermacell Gypsum fibre boards according to ETA-03/0050.

The screws may be used for connecting the following wood-based panels to the timber members mentioned above:

- Plywood according to EN 636⁸ and EN 13986,
- Oriented Strand Board, OSB according to EN 300 and EN 13986,
- Particleboard according to EN 312 and EN 13986,
- Fibreboards according to EN 622-2⁹, EN 622-3¹⁰ and EN 13986,
- Cement-bonded particle boards according to EN 634-2¹¹ and EN 13986,
- Solid-wood panels according to EN 13353 and EN 13986.

Wood-based panels (except OSB, particleboards and solid-wood panels) and steel members shall only be arranged on the side of the screw head.

1	EN 14081-1:2005+A1:2011	Timber structures – Strength graded structural timber with rectangular cross section – Part
2	EN 44000-2012	1: General requirements
2	EN 14080:2013	Timber structures - Glued laminated timber and glued solid timber - Requirements
3	EN 14374:2004	Timber structures - Structural laminated veneer lumber - Requirements
4	EN 300:2006	Oriented strand boards (OSB) – Definition, classification and specifications
5	EN 13986:2004+A1:2015	Wood-based panels for use in construction - Characteristics, evaluation of conformity and marking
6	EN 312:2010	Particleboards - Specifications
7	EN 13353:2008+A1:2011	Solid wood panels (SWP) – Requirements
8	EN 636:2012+A1:2015	Plywood - Specifications
9	EN 622-2:2004	Fibreboards – Specifications – Part 2: Requirements for hardboards
10	EN 622-3:2004	Fibreboards - Specifications - Part 3: Requirements for medium boards
11	EN 634-2:2007	Cement-bonded particleboards – Specifications – Part 2: Requirements for OPC bonded particleboards for use in dry, humid and external conditions

Würth self-tapping screws Annex 1 Specifications of intended use Annex 1



If in a European Technical Assessment according to ETAG 015 screws according to EN 14592 are specified to connect three-dimensional nailing plates, Würth screws according to ETA-11/0190 may be considered equivalent, provided that the assumptions regarding the screws in the ETA according to ETAG 015 are met.

Würth "ASSY plus VG" and "ASSY" screws with full thread may be used for reinforcing of timber structures perpendicular to the grain. Würth "ASSY plus VG" screws and fully threaded "ASSY" screws with an outer thread diameter of d = 8 mm may also be used for shear reinforcement.

Würth screws with an outer thread diameter of at least 6 mm may be used for the fixing of thermal insulation material on top of rafters or on wood-based members in vertical façades.

A.1.3 Use Conditions (environmental conditions)

The corrosion protection of the Würth screws is specified in Annex A.2.6. With regards to the use and the environmental conditions, the national provisions of the place of installation apply.

A.1.4 Installation provisions

EN 1995-1-1¹² in conjunction with the respective national annex applies for the installation.

A minimum of two screws shall be used for connections in load-bearing timber structures. When fixing boards, battens or intermediate connections of wind braces only one screw may be used. This also applies for the fixing of rafters, purlins or similar on main beams or top plates, if the member is fixed with at least two screws in total.

Only one screw may be used in structural connections when the minimum penetration length of the screw is 20 · d and the screw is systematic axially loaded. In the case the screw is used to connect wood-based members the load-bearing capacity of the screw shall be reduced by 50 %. If the screw is used as tensile or compressive reinforcement of timber structures perpendicular to the grain no reduction of the load-bearing capacity of the screw is necessary.

The screws are either driven into the wood-based member made of softwood without pre-drilling or in pre-drilled holes with a diameter according to Table A.1.1.

The screws are driven into wood-based members made of beech, ash or oak except LVL made from beech according to EN 14374 or FST according to ETA-14/0354 in pre-drilled holes with a diameter according to Table A.1.1.

Outer thread diameter	Diameter of the pre-drilled hole with a tolerance of ± 0.1 mm [mm]					
[mm]	Wood-based member of softwood	Wood-based members made of beech, ash or oak				
3.0/ 3.4	1.5	2.0				
3.5/ 3.9	2.0	2.5				
4.0/ 4.4	2.5	3.0				
4.5	2.5	3.5				
5.0	3.0	3.5				
5.5/ 6.0/ 6.3	4.0	4.0				
6.5/ 7.0	4.0	5.0				
7.5/ 8.0	5.0	6.0				
10.0	6.0	7.0				
12.0	7.0	8.0				
14.0	8.0	9.0				

Table A.1.1Diameter of the pre-drilled holes in softwood and in beech, ash or oak

¹² EN 1995-1-1: 2004+AC:2006+A1:2008+A2:2014 Eurocode 5: Design of timber structures – Part 1-1: General - Common rules and rules for buildings

 Würth self-tapping screws
 Annex 1

 Installation provisions
 Annex 1



Würth "ASSY" and "Jamo" screws made from carbon steel may be driven into Beech LVL according to EN 14374 or in FST according to ETA-14/0354 without pre-drilling considering the maximum penetration depth of the screws according to Table A.1.2. Screws made from stainless steel may be driven into members made from softwood with or without pre-drilling.

Table A.1.2 Maximum penetration length of the threaded part of Würth "ASSY" and "Jamo" screws made from carbon steel when driven into Beech LVL according to EN 14374 or in FST according to ETA-14/0354 without pre-drilling

Outer thread diameter	Maximum penetration length of [m	•
[mm] ·	"ASSY" and "Jamo" screws with drill tip	"ASSY", "Jamo" or "Amo" screws without drill tip
5.0	-	50
6.0	30	60
7.0	-	70
7.5	-	75
8.0	48	80
10.0	80	100
12.0	96	-

The screw holes in steel members shall be pre-drilled with an adequate diameter greater than the outer thread diameter.

Würth screws with an outer thread diameter of d = 14 mm and a length greater or equal than 800 mm shall be only driven in softwood in a guiding hole with a diameter of 8 mm and a minimum length of 10 percent of the screw length.

If screws with an outer thread diameter $d \ge 8$ mm are driven into the wood-based member without pre-drilling, the structural solid or glued laminated timber, laminated veneer lumber and similar glued members shall be from spruce, pine, fir or beech (only LVL or FST).

In the case of fastening battens on thermal insulation material on top of rafters the screws shall be driven in the rafter through the battens and the thermal insulation material without pre-drilling in one sequence.

Screws may be used with appropriate washers according to Annex 9. After inserting the screw the washers shall touch the surface of the wood-based member completely.

By fastening screws in wood-based members the head of the screws shall be flush with the surface of the woodbased member. For pan head, top head, back panel head, Elmo-head, large washer head, joist hanger screw head, kombi hexagonal head, truss head, hexagonal head and hexalobular head the head part remains unconsidered.

Spacing, end and edge distances	Annex 1

Würth self-tapping screws



ANNEX 2 – Characteristic values of the load-carrying capacities

Table A.2.1 Characteristic load-carrying capacities of Würth self-tapping screws made from carbon steel with d = 3.0 mm to 6.0 mm

Outer thread diameter [mm]			3.4	3.5	3.9	4.0	4.4	4.5	5.0	6.0
Characteristic yield moment	ASSY plus VG	-	-	-	-	-	-	-	-	10.0
M _{y,k} [Nm]	ASSY 3.0/ plus MDF	-	1.7	-	1.9	-	3.0	-	-	-
	Remaining screws	1.6	-	1.8	-	3.3	-	3.7	5.9	10.0
Characteristic	ASSY plus VG	-	-	-	-	-	-	-	-	12.5
tensile strength	ASSY 3.0/ plus MDF	-	2.8	-	3.9	-	5.0	-	-	-
f _{tens,k} [kN]	Remaining screws	2.8	-	3.0	-	5.0	-	5.3	7.9	12.5
Characteristic torsional strength	ASSY plus VG	-	-	-	-	-	-	-	-	11.5
	ASSY 3.0/ plus MDF	-	1.5	-	1.9	-	3.0	-	-	-
f _{tor,k} [Nm]	Remaining screws	1.5	-	2.0	-	3.0	-	4.3	6.0	10.0

Würth self-tapping screws

Characteristic values of the load-carrying capacities

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Outer thread d	6.3	7.0	7.5	8.0	10.0	12.0	14.0	
Characteristic	ASSY plus VG	-	-	-	23.0	36.0	58.0	86.0
yield moment M _{y,k} [Nm]	ASSY plus VG Hot-dip galvanised	-	-	-	-	-	-	86.0
	ASSY Isotop 8.0/10.0	-	-	-	11.0	-	-	-
	Amo Y	-		21.0				
	WG Fix	6.5		-				
	Remaining screws	-	14.0	-	23.0	36.0	58.0	-
Characteristic	ASSY plus VG	-	-	-	22.0	33.0	45.0	62.0
tensile strength	ASSY plus VG Hot-dip galvanised	-	-	-	-	-	-	47.0
f _{tens,k} [kN]	ASSY Isotop 8.0/10.0	-	-	-	11.0	-	-	-
	Amo Y	-		18.0				
	WG Fix	8.0		-				
	Remaining screws	-	15.0	-	21.5	26.0	41.0	-
Characteristic torsional	ASSY plus VG	-	-	-	25.0	45.0	75.0	115
strength f _{tor,k} [Nm]	ASSY plus VG Hot-dip galvanised	-	-	-	-	-	-	100
	ASSY Isotop 8.0/10.0				20 ^{a)}			
		-	-	-	12 ^{b)}	-	-	-
	Amo Y	-		20.0				
	WG Fix	8.0		-				
	Remaining screws	-	15.0	_	23.0	45.0	65.0	_

Table A.2.2	Characteristic load-carrying capacities of Würth self-tapping screws made from carbon steel with
	d = 6.3 mm to 14.0 mm

 Table A.2.3
 Characteristic load-carrying capacities of Würth self-tapping screws made from stainless steel

Outer thread diameter [mm]		3.0	3.5	4.0	4.5	5.0	5.5	6.0	6.5	8.0	10.0
Characteristic yield moment M _{y,k} [Nm]		0.9	1.4	1.9	2.3	2.8	4.4	5.5	6.8	11.0	20.0
Characteristic tensile strength f _{tens,k} [kN]		1.8	2.4	3.1	3.6	4.2	5.9	7.1	8.3	12.0	19.0
Characteristic torsional strength f _{tor,k} [Nm]	Head side ASSY P screws	-	2.7	-	3.6		6.3	-	-	-	-
	Point side remaining screws	0.85	1.35	2.0	2.6	3.3	5.2	6.4	7.5	16.0	30.0

Würth self-tapping screws

Spacing, end and edge distances



A.2.1 General

The minimum penetration length of the threaded part of the screw in the wood-based members lef shall be

$$I_{ef} = \min \begin{cases} \frac{4 \cdot d}{\sin \alpha} \\ 20 \cdot d \end{cases}$$
(2.1)

where

 α angle between screw axis and grain direction

d outer thread diameter of the screw.

When fastening battens on thermal insulation material on top of rafters the minimum penetration length of the threaded part of the screw in the wood-based members I_{ef} shall be 40 mm, in case of flanges made from LVL 39 mm.

The outer thread diameter of screws inserted in cross-laminated timber shall be at least 6 mm. The inner thread diameter d_1 of the screws shall be greater than the maximal width of the gaps in the layer of cross laminated timber.

Reductions in the cross-sectional area caused of wood-based members by Würth screws with a diameter of 10 mm or more shall be taken into account in the member strength verification both, in the tensile and compressive area of members. For screws in pre-drilled holes, the drill hole diameter should be considered in the member strength verification, for screws driven without pre-drilling, the inner thread diameter.

A.2.2 Laterally loaded screws

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A.2.2.1 General

The outer thread diameter d shall be used as effective diameter of the screw according to EN 1995-1-1.

The embedding strength for the screws in wood-based members or in wood-based panels shall be taken from EN 1995-1-1 or from national provisions that apply at the installation site unless otherwise specified in the following.

For steel-to-timber connections with screws d = 5 mm with joist hanger screw head, a thick steel plate may be assumed for steel plate thickness $t \ge 1,5$ mm.

For laterally loaded screws, the rules for multiple fastener connections in EN 1995-1-1, 8.3.1.1 (8) should be applied, if the timber under each fastener in a connection is not reinforced according to Annex 6.

A.2.2.2 Solid timber, glued laminated timber, glued solid timber and solid wood panels

The embedding strength for screws in non-pre-drilled holes in softwood arranged at an angle between screw axis and grain direction of $0^{\circ} \le \alpha \le 90^{\circ}$ is:

$$f_{h,k} = \frac{0.082 \cdot \rho_k \cdot d^{-0.3}}{2.5 \cdot \cos^2 \alpha + \sin^2 \alpha}$$
 [N/mm²] (2.2)

The embedding strength for screws in pre-drilled holes in softwood or in ash, beech or oak hardwood arranged at an angle between screw axis and grain direction of $0^{\circ} \le \alpha \le 90^{\circ}$ is:

$f_{h,k} = \frac{0.082 \cdot \rho_k \cdot (1 - 0.01 \cdot d)}{2.5 \cdot \cos^2 \alpha + \sin^2 \alpha}$	[N/mm²]		(2.3)
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Würth self-tapping screws	
Characteristic values of the load-carrying capacities	Annex 2



where

 ρ_k Characteristic density of the wood-based member [kg/m³], for beech, ash and oak $\rho_k \le 590$ kg/m³

- d Outer thread diameter of the screw [mm]
- α Angle between screw axis and grain direction, $0^{\circ} \le \alpha \le 90^{\circ}$.

A.2.2.3 Laminated veneer lumber

The embedding strength for screws in non-pre-drilled holes in softwood LVL arranged at an angle between screw axis and grain direction, $0^{\circ} \le \alpha \le 90^{\circ}$ is:

$$f_{h,k} = \frac{0.082 \cdot \rho_k \cdot d^{-0.3}}{(2.5 \cdot \cos^2 \alpha + \sin^2 \alpha)(1.5 \cdot \cos^2 \beta + \sin^2 \beta)}$$
 [N/mm²] (2.4)

and accordingly for screws in pre-drilled holes in softwood LVL arranged at an angle between screw axis and grain direction, $0^{\circ} \le \alpha \le 90^{\circ}$:

$$f_{h,k} = \frac{0.082 \cdot \rho_k \cdot (1 - 0.01 \cdot d)}{(2.5 \cdot \cos^2 \alpha + \sin^2 \alpha)(1.5 \cdot \cos^2 \beta + \sin^2 \beta)}$$
 [N/mm²] (2.5)

Where

 $\rho_k \qquad \text{characteristic timber density of the softwood LVL [kg/m³], } \rho_k \leq 500 \text{ kg/m³},$

d outer thread diameter of the screw [mm],

 α angle between screw axis and grain direction (0° ≤ α ≤ 90°),

 β angle between screw axis and the LVL's wide face (0° ≤ α ≤ 90°).

The embedding strength for screws in pre-drilled or non-pre-drilled holes in Beech LVL according to EN 14374 or in FST according to ETA-14/0354 arranged at an angle between screw axis and grain direction, $0^{\circ} \le \alpha \le 90^{\circ}$ is:

$$f_{h,k} = \frac{0.082 \cdot \rho_k \cdot d^{-0.15}}{(2.5 \cdot \cos^2 \alpha + \sin^2 \alpha) \cdot k_\epsilon \cdot k_\beta}$$
[N/mm²] (2.6)

Where

 ρ_k characteristic density of Beech LVL or FST [kg/m³], $\rho_k \le 730$ kg/m³

d outer thread diameter of the screw [mm],

 α angle between screw axis and grain direction, $0^{\circ} \leq \alpha \leq 90^{\circ}$,

$$\mathbf{k}_{\varepsilon} = (0.5 + 0.024 \cdot \mathbf{d}) \cdot \sin^2 \varepsilon + \cos^2 \varepsilon, \qquad (2.7)$$

 ϵ angle between load and grain direction, $0^{\circ} \le \epsilon \le 90^{\circ}$,

$$k_{\beta} = 1.2 \cdot \cos^2 \beta + \sin^2 \beta, \qquad (2.8)$$

 β angle between screw axis and wide face of LVL or FST member, $0^{\circ} \le \beta \le 90^{\circ}$.

Würth self-tapping screws	
Characteristic load-bearing capacity values	Annex 2



A.2.2.4 Cross laminated timber

The embedding strengths according to equations (2.2) and (2.3) may be applied for screws within single softwood layers in cross laminated timber, if the single layer is considered as a separate softwood member and the minimum spacing, end and edge distances are observed for the single layer. For inner layers, the edge distance perpendicular to the grain may be reduced to $3 \cdot d$.

Alternatively the embedding strength for screws arranged in the edge surfaces parallel to the plane of cross laminated timber may be assumed according to equation (2.9) independent of the angle between screw axis and grain direction, $0^{\circ} \le \alpha \le 90^{\circ}$:

$$f_{h,k} = 20 \cdot d^{-0.5}$$
 in N/mm²

unless otherwise specified in the technical specification of the cross laminated timber.

Where d is the outer thread diameter of the screws in mm.

Equation (2.9) is only valid for softwood layers. The provisions in the European Technical Assessment or in national provisions of the cross laminated timber apply.

The embedding strength for screws in the wide face of cross laminated timber may be assumed as for solid timber based on the characteristic density of the outer layer. Where applicable, the angle between force and grain direction of the outer layer shall be taken into account. The direction of the lateral force shall be perpendicular to the screw axis and parallel to the wide face of the cross laminated timber.

A.2.3 Axially loaded screws

A.2.3.1 Axial slip modulus

The axial slip modulus K_{ser} of the threaded part of a screw for the serviceability limit state shall be taken independent of angle α to the grain as:

$K_{ser} = 25 \cdot d \cdot I_{ef} [N/mm]$	for screws in members made from softwood	(2.10)
$K_{ser} = 30 \cdot d \cdot I_{ef}$ [N/mm]	for screws in in members made from hardwood	(2.11)

Where

d outer thread diameter of the screw [mm]

l_{ef} penetration length of the of the threaded part of the screw in the wood-based member [mm].

A.2.3.2 Axial withdrawal capacity

The characteristic withdrawal capacity in solid timber (softwood or hardwood species beech, ash and oak with $\rho_k \le 590 \text{ kg/m}^3$), glued laminated timber (softwood or hardwood species beech, ash and oak with $\rho_k \le 590 \text{ kg/m}^3$), cross laminated timber, solid wood panels or laminated veneer lumber members or FST according to ETA-14/0354 with $\rho_k \le 750 \text{ kg/m}^3$ at an angle of $0^\circ \le \alpha \le 90^\circ$ to the grain shall be calculated as:

$$F_{ax,\alpha,Rk} = \frac{n_{ef} \cdot k_{ax} \cdot f_{ax,k} \cdot d \cdot I_{ef}}{k_{\beta}} \cdot \left(\frac{\rho_{k}}{\rho_{a}}\right)^{0.8}$$
(2.12)

where

n_{ef}

 $F_{ax,\alpha,Rk}$ characteristic withdrawal capacity of a screw group at an angle a to the grain [N]

effective number of screws according to EN 1995-1-1, clause 8.7.2 (8)

For inclined screws in laterally loaded connections with an angle between shear plane and screw axis $30^{\circ} \le \alpha \le 60^{\circ}$:

$$n_{ef} = max \left\{ n^{0.9}; 0.9 \cdot n \right\}$$

Alternatively, the effective number of inclined screws with an angle α between shear plane and screw axis of 30° $\leq \alpha \leq 60^{\circ} n_{ef}$ may be determined according to Annex 8.

For screws as compression reinforcement or inclined screws as fasteners in mechanically jointed beams or columns or for the fixing of thermal insulation material, $n_{ef} = n$.

Würth self-tapping screws

Characteristic load-bearing capacity values

Annex 2

(2.9)

(2.13)



n	number of screws acting together in a connection
	For inclined screws is n the number of crossed pairs of screws.
k _{ax}	Factor, taking into account the angle $lpha$ between screw axis and grain direction
	$k_{ax} = 1.0$ for $45^\circ \le \alpha \le 90^\circ$
	$k_{ax} = a + \frac{b \cdot \alpha}{45^{\circ}} \qquad \text{for } 0^{\circ} \le \alpha < 45^{\circ} \qquad (2.14)$
	$a = \begin{cases} 0.5 \text{ for LVL} \\ 0.3 \text{ for solid timber, glued solid timber, glued laminated timber, cross laminated timber and solid wood panels} \end{cases}$
	$b = \begin{cases} 0.5 \text{ for LVL} \\ 0.7 \text{ for solid timber, glued solid timber, glued laminated timber, cross laminated timber and solid wood panels} \end{cases}$
	If $l_{ef} \ge \min \begin{cases} \frac{4 \cdot d}{\sin \alpha} \\ \alpha \ge 15^{\circ} k_{ax} \text{ may alternatively be taken as} \end{cases}$
	$k_{ax} = \frac{1}{1.2 \cdot \cos^2 \alpha + \sin^2 \alpha} $ (2.15)
1.	
k_{β}	k_{β} = 1.0 for solid timber, glued solid timber, glued laminated timber and solid wood panels
	$k_{\beta} = 1.5 \cdot \cos^{2}\beta + \sin^{2}\beta \qquad \text{for laminated veneer lumber} $ (2.16)
$f_{ax,k}$	characteristic withdrawal parameter for
	 solid timber, glued laminated timber, cross laminated timber, solid wood panels and laminated veneer lumber members with a maximum characteristic density of 590 kg/m³ and ρ_a = 350 kg/m³
	$f_{ax,k} = 12.0 \text{ N/mm}^2$ for screws with 3.0 mm $\leq d \leq 5.0 \text{ mm}$
	$f_{ax,k} = 11.5 \text{ N/mm}^2$ for screws with 5.5 mm $\leq d \leq 7.0$ mm and "ASSY Isotop" screws
	$f_{ax,k} = 11.0 \text{ N/mm}^2$ for screws with 7.5 mm $\leq d \leq 10.0 \text{ mm}$ and "ASSY plus MDF" screws
	$f_{ax,k} = 10.0 \text{ N/mm}^2$ for screws with d > 10.0 mm and "WG Fix" screws.
	• Beech LVL or FST (ETA-14/0354) members with a density of 590 kg/m³ $\leq \rho_k \leq$ 750 kg/m³ and ρ_a = 730 kg/m³
	$f_{ax,k} = 35.0 \text{ N/mm}^2$ for screws with 5.0 mm $\leq d \leq 12.0 \text{ mm}$
	• OSB/3, OSB/4 boards with $\rho_k \ge 550 \text{ kg/m}^3$ and particleboards with $\rho_k \ge 640 \text{ kg/m}^3$ and $\rho_a = \rho_k f_{ax,k} = 7.0 \text{ N/mm}^2$ for screws with 4.0 mm $\le d \le 6.0 \text{ mm}$
	• Gypsum fibre boards (ETA-03/0050) and gypsum plasterboards with $\rho_k \ge 650$ kg/m ³ and $\rho_a = \rho_k$
	$f_{ax,k} = 7.0 \text{ N/mm}^2$ for "WG Fix" screws in gypsum fibre boards $f_{ax,k} = 2.0 \text{ N/mm}^2$ for "WG Fix" screws in gypsum plasterboards

 Würth self-tapping screws
 Annex 2

 Characteristic load-bearing capacity values
 Annex 2



d outer thread diameter of the screw	/ [mm]
--------------------------------------	--------

l_{ef} penetration length of the threaded part of the screw [mm]

- α angle between grain and screw axis (0° ≤ α ≤ 90°)
- β angle between screw axis and the LVL's wide face ($0^\circ \le \alpha \le 90^\circ$)
- ρ_k characteristic density of the wood-based member or of the gypsum fibre boards or plasterboards [kg/m³]
- ρ_a associated density for f_{ax,k} [kg/m³]

The characteristic withdrawal parameter is also valid for softwood layers of cross-laminated timber.

For screws penetrating more than one layer of cross laminated timber the different layers may be taken into account proportionally. In the lateral surfaces of the cross laminated timber the screws shall be fully inserted in one layer of cross-laminated timber.

Alternatively, the axial withdrawal capacity for screws arranged parallel to the plane of cross laminated timber, independent of the angle between screw axis and grain direction, $0^{\circ} \le \alpha \le 90^{\circ}$, may be calculated from:

$$F_{ax,Rk} = 20 \cdot d^{0.8} \cdot l_{ef}^{0.9}$$
 [N]

Where

d outer thread diameter [mm]

I_{ef} penetration length of the threaded part of the screw [mm]

For beech, ash and oak wood except Beech LVL and FST (ETA-14/0354) a maximum characteristic density of 590 kg/m³ shall be used in equation (8.40a) of EN 1995-1-1 and in equation (2.12) of this ETA.

The axial withdrawal capacity is limited by the head pull-through capacity and the tensile or compressive capacity of the screw.

A.2.3.3 Head pull-through capacity

The characteristic value of the head pull-through parameter for the screws for $\rho_a = 350 \text{ kg/m}^3$ of the timber and for wood-based panels like

- Plywood according to EN 636 and EN 13986
- Oriented Strand Board, OSB according to EN 300 and EN 13986
- Particleboard according to EN 312 and EN 13986
- Fibreboards according to EN 622-2, EN 622-3 and EN 13986
- Cement-bonded particle boards according to EN 634-2 and EN 13986,
- Solid-wood panels according to EN 13353 and EN 13986

with a thickness of more than 20 mm is

$f_{head,k} = 13.0 \text{ N/mm}^2$	for Würth screws with a head diameter $d_h \le 19$ mm and
$f_{head,k} = 10.0 \text{ N/mm}^2$	for Würth screws with a head or washer diameter $d_h > 19$ mm,
$f_{head,k} = 15.0 \text{ N/mm}^2$	for Würth "JAMO" and "JAMO plus" screws,
$f_{head,k} = 23.0 \text{ N/mm}^2$	for Würth "ASSY" screws with underhead thread,
$f_{head,k} = 40 - 0.5 \cdot d_h$	for Würth screws with a head or washer diameter $d_h \le 25 \text{ mm}$ in Beech LVL or FST (ETA-14/0354) with a characteristic density of 590 kg/m ³ $\le \rho_k \le 750 \text{ kg/m}^3$ and with a thickness of at least 40 mm,
$f_{head,k}$ = 16.0 N/mm ²	for Würth screws with d = 8 mm with countersunk washers 45° with d_{head} = 25 mm in LVL with $\rho_k \le 590 \text{ kg/m}^3$ for ρ_a = 500 kg/m ³
$f_{head,k} = 32.0 \text{ N/mm}^2$	for Würth screws d = 8 mm with countersunk washers 45° with d _{head} = 25 mm in Beech LVL or FST (ETA-14/0354) with $\rho_k \ge 680 \text{ kg/m}^3$ for $\rho_a = 730 \text{ kg/m}^3$ and with a thickness of at least 40 mm.

Würth self-tapping screws	
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(2.17)



For wood-based panels a maximum characteristic density of 380 kg/m³ and for beech, ash and oak wood and LVL made from softwood a maximum characteristic density of 590 kg/m³ shall be used in equation (8.40b) of EN 1995-1-1. For Beech LVL and FST (ETA-14/0354) a maximum characteristic density of 730 kg/m³ shall be used in equation (8.40b) of EN 1995-1-1.

The head diameter shall be equal to or greater than $1.8 \cdot d_s$, where d_s is the smooth shank or the inner thread diameter. Otherwise the characteristic head pull-through capacity in equation (8.40b) of EN 1995-1-1 is for all wood-based materials: $F_{ax,\alpha,RK} = 0$.

For wood based panels with a thickness $12 \text{ mm} \le t \le 20 \text{ mm}$ the characteristic value of the head pull-through parameter for the screws is:

 $f_{head,k} = 8 \text{ N/mm}^2$

For wood based panels with a thickness of less than 12 mm the characteristic head pull-through capacity for screws shall be based on a characteristic value of the head pull-through parameter of 8 N/mm², and limited to 400 N complying with the minimum thickness of the wood based panels of 1.2·d, with d as outer thread diameter and the values in Table A.2.4.

 Table A.2.4 Minimum thickness of wood based panels

Wood based panel	Minimum thickness [mm]		
Plywood	6		
Fibreboards (hardboards and medium boards)	6		
Oriented Strand Boards, OSB	8		
Particleboards	8		
Cement-bonded particle board	8		
Solid wood Panels	12		

Outer diameter of washers $d_h > 32$ mm shall not be considered.

For Würth "ASSY plus VG" screws, "ASSY" screws with a full thread and "ASSY" screws with a thread under the head the withdrawal capacity of the thread in the wood-based member with the screw head may be taken into account instead of the head pull-through capacity.

That also applies for screws with a thread over a part of the screw length. The minimum penetration length of the thread of $4 \cdot d$ shall be considered in the timber member near the screw head in this case.

In steel-to-timber connections the head pull-through capacity is not governing.

Würth self-tapping screws

Characteristic load-bearing capacity values



A.2.3.4 Compressive capacity of Würth "ASSY plus VG" screws and fully threaded "ASSY" screws

The design axial capacity Fax,Rd of Würth "ASSY plus VG" screws and fully threaded "ASSY" screws embedded in solid timber, glued solid timber or glued laminated timber made from softwood with an angle between screw axis and grain direction of $30^{\circ} \le \alpha \le 90^{\circ}$ is the minimum of the axial resistance against pushing-in and the buckling resistance of the screw.

$$\begin{split} F_{ax,Rd} &= \min \left\{ f_{ax,d} \cdot d \cdot I_{ef}; \kappa_{c} \cdot N_{pl,d} \right\} \eqno(2.18) \\ f_{ax,d} & \text{design value of the axial withdrawal capacity of the threaded part of the screw [N/mm2]} \\ d & \text{outer thread diameter of the screw [mm]} \\ I_{ef} & \text{penetration length of the threaded part of the screw in the timber member [mm]} \\ \kappa_{c} &= 1 & \text{for } \overline{\lambda}_{k} \leq 0.2 & (2.19) \\ \kappa_{c} &= \frac{1}{k + \sqrt{k^{2} - \overline{\lambda}_{k}^{2}}} & \text{for } \overline{\lambda}_{k} > 0.2 & (2.20) \\ k &= 0.5 \cdot \left[1 + 0.49 \cdot \left(\overline{\lambda}_{k} - 0.2 \right) + \overline{\lambda}_{k}^{2} \right] & (2.21) \end{split}$$

and a relative slenderness ratio
$$\overline{\lambda}_{k} = \sqrt{\frac{N_{pl,k}}{N_{kl,k}}}$$
 (2.22)

where:

_

N_{pl,k} characteristic plastic normal force related to the net cross-section of the inner thread diameter: :

$$N_{pl,k} = \pi \cdot \frac{d_1^2}{4} \cdot f_{y,k}$$
(2.23)

characteristic yield strength, f_{y,k}

 $f_{y,k}$ = 1000 N/mm² for "ASSY plus VG" and fully threaded "ASSY" screws

f_{v.k} = 800 N/mm² for hot-dip galvanised "ASSY" plus VG screw

inner thread diameter of the screw [mm] d₁

$$N_{pl,d} = \frac{N_{pl,k}}{\gamma_{M1}}$$
(2.24)

partial factor according to EN 1993-1-1 in conjunction with the particular national annex γ_{M1} characteristic ideal elastic buckling load:

$$N_{ki,k} = \sqrt{c_h \cdot E_S \cdot I_S} \quad [N]$$
(2.25)

elastic foundation of the screw:

$$c_{h} = (0.19 + 0.012 \cdot d) \cdot \rho_{k} \cdot \left(\frac{90^{\circ} + \alpha}{180^{\circ}}\right) [N/mm^{2}]$$
 (2.26)

characteristic density of the wood-based member [kg/m³], ρ_k

angle between screw axis and grain direction, α

modulus of elasticity:

E_s = 210.000 N/mm²

second moment of area:

$$I_{s} = \frac{\pi \cdot d_{1}^{4}}{64} \qquad [mm^{4}]$$
 (2.27)

Würth self-tapping screws

Characteristic values of the load-carrying capacities



A.2.4 Spacing, end and edge distances of the screws and minimum thickness of the wood and gypsum based material

A.2.4.1 General

For screws arranged at angles α < 90° between screw axis and grain direction minimum spacing and distances are defined as follows:

Minimum spacing a_1 or a_2 is defined perpendicular to the screw axis, minimum end or edge distances $a_{1,t,CG}$, $a_{1,c,CG}$, $a_{2,c,CG}$ und $a_{2,t,CG}$ parallel or perpendicular to the grain, respectively, are defined between the centre of the threaded screw length (axial loading) or the screw length (lateral loading) in the respective timber member and the member surface as for axially loaded screws in Figure 8.11.a in EN 1995-1-1.

A.2.4.2 Laterally and/or axially loaded screws

Screws in pre-drilled holes or "ASSY plus", "ASSY plus VG" and "Jamo plus"¹³ screws in non-predrilled holes. For Würth screws in pre-drilled holes, for "ASSY plus", "ASSY plus VG" and "Jamo plus"¹³ screws also in non pre-drilled holes in softwood, the minimum spacings, end and edge distances are given in EN 1995-1-1, clause 8.3.1.2 and Table 8.2 as for nails in pre-drilled holes. Here, the outer thread diameter d shall be considered.

Minimum thickness for structural members made from solid timber, glued laminated timber, glued solid timber, laminated veneer lumber and cross laminated timber is t = 24 mm for screws with d < 8 mm, t = 30 mm for screws with d = 8 mm, t = 40 mm for screws with d = 10 mm, t = 80 mm for screws with d = 12 mm and t = 100 mm for screws with d = 14 mm.

Minimum thickness for OSB/3, OSB/4 boards is 12 mm and for particle boards 13 mm. The thickness of the boards shall not be greater than 30 mm. The minimum thickness of wood-based panels arranged on the side of the screw head is given in Table A.2.4.

The minimum thickness of gypsum plasterboards is 12.5 mm and for fermacell Gypsum fibre boards 10 mm.

Screws in non pre-drilled holes

For Würth screws except for "ASSY plus" "ASSY plus VG" and "Jamo plus" screws in non pre-drilled holes minimum spacing and distances are given in EN 1995-1-1, clause 8.3.1.2 and Table 8.2 as for nails in non pre-drilled holes. Minimum spacing and distances according to EN 1995-1-1, clause 8.3.1.2 and Table 8.2 for nails in non pre-drilled holes and a characteristic density of 420 kg/m³ $\leq \rho_k \leq 500$ kg/m³ also apply for "ASSY", "Jamo" and "Amo" screws made from carbon steel with 5 mm $\leq d \leq 12$ mm in Beech LVL and FST (ETA-14/0354) for type S with member thickness t $\geq 7 \cdot d$ and for type Q independent of the member thickness.

For Douglas fir members minimum spacing and distances parallel to the grain shall be increased by 50%.

Minimum distances from the unloaded edge perpendicular to the grain may be reduced to $3 \cdot d$ also for timber thickness t < $5 \cdot d$, if the spacing parallel to the grain and the end distance is at least $25 \cdot d$.

For Würth screws in non-predrilled softwood members except "ASSY plus", "ASSY plus VG" and "Jamo plus" the minimum member thickness defined in EN 1995-1-1, clause 8.3.1.2 as for nails in non-predrilled holes is valid. Equation (8.18) in EN 1995-1-1 may be applied for softwood members made of pine or for the fixing of boards, battens or wind braces, if the member is fixed with at least two screws. Otherwise EN 1995-1-1, clause 8.3.1.2 (7) applies.

¹³ The spacings and distances given in this paragraph are only valid for "Jamo plus" screws if the screws are inserted only until the end of the smooth shaft. The spacings and distances are not valid for the underhead thread of the "Jamo plus" screws.

Würth self-tapping screws

Spacing, end and edge distances



If the spacing parallel to the grain and the end distance is at least $25 \cdot d$ or if the timber in the connection area is reinforced according to Annex 8, the minimum thickness for predrilled structural members or for "ASSY plus" and "ASSY plus VG" screws in non-predrilled softwood members may be reduced to t = 24 mm for screws with outer thread diameter d < 8 mm, to t = 30 mm for screws with outer thread diameter d = 8 mm, to t = 40 mm for screws with outer thread diameter d = 10 mm, to t = 80 mm for screws with outer thread diameter d = 12 mm and to t = 100 mm for screws with outer thread diameter d = 14 mm.

These minimum member thicknesses are not valid for wood-based panels and LVL with cross veneers.

A.2.4.3 Only axially loaded screws

For "ASSY plus", "ASSY plus VG" and "Jamo plus"¹³ screws loaded only axially, the following minimum spacings, end and edge distances may be used alternatively to paragraph A.2.4.2 for solid timber, glued laminated timber and similar glued products:

Spacing a_1 in a plane parallel to grain:	a ₁	= 5 · d
Spacing a ₂ perpendicular to a plane parallel to grain:	a ₂	= 2.5 · d
End distance $a_{1,CG}$ of the centre of gravity of the threaded part		
in the timber member:	$a_{1,CG}$	= 5 · d
Edge distance a _{2,CG} of the centre of gravity of the threaded part		
in the timber member:		= 3 · d
Product of spacing a_1 and a_2 :	$a_1 \cdot a_2$	$= 25 \cdot d^2$

For screws in non pre-drilled holes a minimum timber thickness of 10 d and a minimum width of 8 d or 60 mm, whichever is the greater, are required.

For "ASSY plus" and "ASSY plus VG" and "Jamo plus"¹³ screws only loaded axially, the following minimum spacings, end and edge distances apply for laminated veneer lumber (LVL) made from softwood:

S	pacing a₁ in a plane parallel to grain:	a ₁	= 5 · d
S	pacing a_2 perpendicular to a plane parallel to grain:	a ₂	= 2.5 · d
	nd distance a _{1,CG} of the centre of gravity of the threaded part to the timber member:	a _{1,CG}	= 5 · d
	dge distance a _{2,CG} of the centre of gravity of the threaded part to the timber member:	a _{2,CG}	= 3 · d
Ρ	roduct of spacing a_1 and a_2 :	$a_1 \cdot a_2$	= $25 \cdot d^2$
_			

For screws in non pre-drilled holes a minimum LVL (softwood) thickness of 6 d and a minimum width of 8 d or 60 mm, whichever is the greater, are required.

For a crossed screw couple in solid timber, glued laminated timber and similar glued products or in laminated veneer lumber the minimum spacing between the crossing screws is 1.5.d. Appropriate means have to ensure that the crossed screws threads do not touch each other when being inserted in the timber member.

A.2.4.4 Cross laminated timber

The minimum requirements for spacing, end and edge distances of screws in the plane or edge surfaces of cross laminated timber are summarised in Table A.2.5. The definition of spacing, end and edge distance is shown in Figure A.2.2 and Figure A.2.3. The minimum spacing, end and edge distances in the edge surfaces are independent of the angle between screw axis and grain direction. They may be used based on the following conditions:

- Minimum thickness of cross laminated timber: 10 · d
- Minimum penetration depth in the edge surface: 10 · d

Würth self-tapping screws	Annex 2
Spacing, end and edge distances	



Unless a detailed verification is carried out the tensile stresses perpendicular to the grain shall be transferred by reinforcing screws for load components perpendicular to the plane surface (see Figure A.2.1),



Figure A.2.1: Reinforcing screw in cross-laminated timber loaded by tensile stress perpendicular to the grain

Table A.2.5 Minimum spacing, end and edge distances of screws in the plane or edge surfaces of cross laminated timber

	a ₁	a _{3,t}	a _{3,c}	a ₂	a _{4,t}	a _{4,c}
Plane surface (see Figure A.2.2)	4 · d	6 · d	6 · d	2.5 · d	6 ⋅ d	2.5 · d
Edge surface (see Figure A.2.3)	10 · d	12 · d	7 · d	4 · d	6 ⋅ d	3 · d

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Figure A.2.2: Definition of spacing, end and edge distances in the plane surface



Figure A.2.3: Definition of spacing, end and edge distances in the edge surface

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A.2.5 Insertion moment

The ratio between the characteristic torsional strength $f_{tor,k}$ and the mean value of insertion moment $R_{tor,mean}$ fulfills the requirement for all screws.

A.2.6 Durability against corrosion

Screws and washers made from carbon steel may be uncoated, brass-plated; nickel-plated; browned; zinc plated; zinc plated blue passivated, yellow chromated, black chromated; zinc-nickel plated, zinc-nickel plated passivated; zinc flakes; ruspert; completly or partially painted, aluminium coating; phosphated; HCP coated, delta coated - surface coatings may be combined together. Würth ASSY plus VG with d = 14 mm may be hot-dip galvanised.

The minimum thickness of the zinc coating of the screws is 5 μm and of the zinc-nickel coating 4 $\mu m.$

Steel no. 1.4006, 1.4009, 1.4021, 1.4301, 1.4401, 1.4529, 1.4571, 1.4567, 1.4578 and 1.4539 is used for screws and washers made from stainless steel.

Contact corrosion shall be avoided.

Würth self-tapping screws

Insertion moment and durability against corrosion



ANNEX 3 Compression reinforcement perpendicular to the grain

A.3.1 General

Only Würth "ASSY plus VG" and "ASSY" screws with full thread shall be used for compression reinforcement perpendicular to the grain. The provisions are valid for reinforcing timber members made from solid timber, glued solid timber and glued laminated timber made from softwood.

The compression force shall evenly be distributed to the screws used as compression reinforcement.

The screws are driven into the timber member perpendicular to the contact surface under an angle between the screw axis and the grain direction of 45° to 90°. The screw heads must be flush with the timber surface.

Compressive reinforcing screws for wood-based panels and timber members made of hardwood are not covered by this European Technical Assessment.

A.3.2 Design

For the design of reinforced contact areas the following conditions must be met independently of the angle between the screw axis and the grain direction.

The design resistance of a reinforced contact area is:

$$\mathsf{R}_{90,d} = \min\left\{ \begin{array}{l} \mathsf{k}_{c,90} \cdot \mathsf{B} \cdot \ell_{ef,1} \cdot \mathsf{f}_{c,90,d} + \mathsf{n} \cdot \min\left\{\mathsf{R}_{ax,d}; \kappa_c \cdot \mathsf{N}_{pl,d}\right\} \\ \mathsf{B} \cdot \ell_{ef,2} \cdot \mathsf{f}_{c,90,d} \end{array} \right\}$$
(3.1)

where:

k_{c,90} parameter according to EN 1995-1-1, clause 6.1.5

B bearing width [mm]

 $\ell_{ef,1}$ effective contact length according to EN 1995-1-1, clause 6.1.5 [mm]

 $f_{c,90,d}$ design compressive strength perpendicular to the grain [N/mm²]

n number of reinforcing screws, $n = n_0 \cdot n_{90}$

n₀ number of reinforcing screws arranged in a row parallel to the grain

n₉₀ number of reinforcing screws arranged in a row perpendicular to the grain

 $R_{ax,d} = f_{ax,d} \cdot d \cdot \ell_{ef}$ [N]

f_{ax,d} design value of the axial withdrawal capacity of the threaded part of the screw [N/mm²]

d outer thread diameter of the screw [mm]

- κ_c according to Annex 2, chapter "compressive capacity"
- $N_{\text{pl,d}}$ according to Annex 2, chapter "compressive capacity" [N]

 $\ell_{ef,2}$ effective contact length in the plane of the screw tips (see Figure 3.1) [mm]

 $\ell_{ef,2} = \{\ell_{ef} + (n_0 - 1) \cdot a_1 + min(\ell_{ef}; a_{1,C})\}$ for end supports (see Figure 3.1 left)

 $\ell_{ef,2} = \{2 \cdot \ell_{ef} + (n_0 - 1) \cdot a_1\}$ for intermediate supports (see Figure 3.1 right)

 ℓ_{ef} penetration length of the threaded part of the screw in the timber member [mm]

 a_1 spacing a_1 in a plane parallel to grain, see chapter A.2.4.3 [mm]

a_{1,C} end distance of the centre of gravity of the threaded part in the timber member, see chapter A.2.4.3 [mm]

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(3.2)

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Figure A.3.1 Reinforced end support (left) and reinforced intermediate support (right)

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 Compression reinforcement perpendicular to the grain
 Annex 3





ANNEX 4 Tensile reinforcement perpendicular to grain

A.4.1 General

Only Würth "ASSY plus VG" and "ASSY" screws with full thread shall be used for tensile reinforcement perpendicular to the grain.

The screws are driven into the timber member perpendicular to the contact surface under an angle between the screw axis and the grain direction of 90°.

The provisions regarding tensile reinforcement perpendicular to the grain are valid for the following timber members:

- solid timber of softwood or of the hardwood species beech, ash or oak,
- glued laminated timber made of softwood or of the hardwood species beech, ash or oak,
- glued solid timber made of softwood or of the hardwood species beech, ash or oak,
- laminated veneer lumber made of softwood.

For the design and construction of the tensile reinforcement of timber members perpendicular to the grain, the provisions at the place of installation shall apply. As examples connection forces at an angle to the grain and notched beam supports are given in the following.

Note: For example, in Germany the provisions of standard DIN EN 1995-1-1/NA:2013-08, NCI NA.6.8 and amendments shall be taken into account.

A minimum of two screws shall be used for tensile reinforcement perpendicular to the grain. Only one screw may be used when the minimum penetration depth of the screws below and above the potential crack is $20 \cdot d$ where d is the outer thread diameter of the screw.

A.4.2 Design

A.4.2.1 Connection forces at an angle to the grain

The axial capacity of a reinforcement of a timber member loaded by a connection force perpendicular to the grain shall fulfil the following condition:

$$\frac{\left[1-3\cdot\alpha^{2}+2\cdot\alpha^{3}\right]\cdot\mathsf{F}_{90,d}}{\mathsf{F}_{ax,Rd}} \le 1$$
(4.1)

where

 $F_{90,d}$ design value of the force component perpendicular to the grain,

 $\alpha = a/h$

a see Figure A.4.1

h = member depth

 $F_{ax,Rd} = min \{ f_{ax,d} \cdot d \cdot I_{ef}; F_{t,Rd} \}$

f_{ax,d} design value of the axial withdrawal capacity of the threaded part of the screw

d outer thread diameter of the screw

I_{ef} smaller value of the penetration depth below or above the potential crack

 $F_{t,Rd}$ design value of the tensile resistance of the screw = $f_{tens,d}$

Outside the connection only one screw each in longitudinal direction of the beam shall be taken into account.

Würth self-tapping screws	
Tensile reinforcement perpendicular to the grain	Annex 4





Figure A.4.1: Example for tensile reinforcement of a connection force perpendicular to the grain

Würth self-tapping screws

Tensile reinforcement perpendicular to the grain



(4.2)

A.4.2.1 Notched beam supports

The axial capacity of a reinforcement of a notched beam support shall fulfil the following condition:

$$\frac{1.3 \cdot V_{d} \cdot \left[3 \cdot (1-\alpha)^{2} - 2 \cdot (1-\alpha)^{3}\right]}{F_{ax,Rd}} \leq 1$$

where

 V_d design value of the shear force

 $\alpha = h_e/h$

h = member depth

 $F_{ax,Rd} = min \{ f_{ax,d} \cdot d \cdot I_{ef}; F_{t,Rd} \}$

 $f_{ax,d}$ design value of the axial withdrawal capacity of the threaded part of the screw

d outer thread diameter of the screw

 I_{ef} smaller value of the penetration depth below or above the potential crack, the total minimum penetration depth of the screw shall be 2 \cdot I_{ef}

 $F_{t,Rd}$ design value of the tensile resistance of the screws = $f_{tens,d}$

Only one screw in longitudinal direction of the beam shall be taken into account.



Figure A.4.2: Example for tensile reinforcement of a notched beam support

Würth self-tapping screws	
Tensile reinforcement perpendicular to the grain	Annex 4



ANNEX 5 Shear reinforcement

A.5.1 General

Only fully threaded Würth "ASSY" and "ASSY plus VG" screws with d = 8 mm may be used for shear reinforcement of timber members. The provisions are valid for straight beams with constant rectangular cross-section.

The screws shall be driven into the timber member under an angle between the screw axis and the grain direction of 45°.

The provisions regarding shear reinforcement are valid for the following timber members:

- Glued laminated timber made of softwood and _
- Glued solid timber made of softwood.

A minimum number of four screws shall be arranged in a line parallel to the grain as shear reinforcement. The spacing between the screws in a line parallel to the grain shall not exceed the depth h of the timber member.

For spacing, end and edge distances of the screws the provisions in Annex A.2.4 apply.

If the screws are arranged in one line parallel to the grain, it shall be done centrically in relation to the beam width.

Outside reinforced areas the shear design shall fulfil the conditions for unreinforced timber members.

For the design and construction of the shear reinforcement of timber members perpendicular to the grain, the provisions at the place of installation shall apply.



Figure A.5.1: Principle of a shear reinforced beam using screws; marked area is reinforced

A.5.2 Design

The provisions are valid for concentrated and linear loads.

For shear in reinforced areas of timber members specified in Annex A.5.1 with a stress component parallel to the grain, the following expression shall be satisfied:

$$\tau_{d} \leq f_{v, \text{mod}, d} = \frac{f_{v, d} \cdot k_{\tau}}{\eta_{H}}$$
(5.1)

where

τ _d	design shear stress [N/mm ²]	
$f_{v,d}$	design shear strength [N/mm ²]	
k_{τ}	$k_{\tau} = 1 - 0.46 \cdot \sigma_{90,d} - 0.052 \cdot \sigma_{90,d}^2 \text{ [N/mm^2]}$	(5.2)

design stress perpendicular to the grain (negative value for compression) [N/mm²]

 $\sigma_{90,d}$

$$\sigma_{90,d} = \frac{F_{ax,d}}{\sqrt{2} \cdot b \cdot a_1}$$
(5.3)

b width of the timber member [mm]

. . .

screw spacing parallel to grain, screws arranged in one row, $a_1 < h$ [mm] a₁

$$F_{ax,d} \qquad F_{ax,d} = \frac{\sqrt{2} \cdot (1 - \eta_H) \cdot V_d \cdot a_1}{h} \qquad [N/mm^2] \qquad (5.4)$$

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$$\eta_{H} = \frac{G \cdot b \cdot 2 \cdot \sqrt{2} \left(\frac{6}{\pi \cdot d \cdot h \cdot k_{ax}} + \frac{a}{E \cdot x} \right)}{1 + G \cdot b \cdot 2 \cdot \sqrt{2} \left(\frac{6}{\pi \cdot d \cdot h \cdot k_{ax}} + \frac{a}{E} \right)}$$

V_d design shear force [N]

d outer thread diameter of the screw [mm]

h depth of the timber member [mm]

G mean value of shear modulus [N/mm²]

k_{ax} connection stiffness between screw and timber member

 $k_{ax} = 12.5 \text{ N/mm}^3$ for fully threaded "ASSY plus VG" and fully threaded "ASSY" screws with d = 8 mm E $\cdot A_S$ Axial stiffness of one screw

$$\mathsf{E} \cdot \mathsf{A}_{\mathsf{S}} = \frac{\mathsf{E} \cdot \pi \cdot \mathsf{d}_{1}^{2}}{4} \tag{5.6}$$

E modulus of elasticity, E = 210.000 N/mm²

d₁ inner thread diameter of the screw [mm]

The axial capacity of a Würth "ASSY plus VG" screw shall fulfil the following condition:

 $\frac{F_{ax,d}}{F_{ax,Rd}} \le 1$ (5.7)

where

 $F_{ax,Rd} = \min \left\{ f_{ax,d} \cdot d \cdot I_{ef}; f_{tens,d} \right\}$

 f_{ax,d}
 design value of the axial withdrawal capacity of the threaded part of the screw [N/mm²]

 l_{ef}
 The effective penetration length is 50 percent of the threaded part length of the screw in the timber member [mm]

 f
 design tappile strength of the screw [N]

f_{tens,d} design tensile strength of the screw [N]

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Shear reinforcement	Annex 5

(5.5)



ANNEX 6 Reinforcement of connections with laterally loaded dowel-type fasteners

Unless specified otherwise in national provisions that apply at the installation site, the axial capacity of a reinforcement of a steel-to-timber or timber-to-timber connection with laterally loaded dowel-type fasteners loaded by a connection force parallel to the grain shall fulfil the following condition:

$$\frac{0.3 \cdot F_{v,0,Ed}}{F_{ax,Rd}} \le 1$$
(6.1)

Where

 $F_{v,0,Ed}$ Design value of the fastener force component parallel to the grain [N],

For outer timber members $F_{v,0,Ed}$ is the load per fastener per shear plane, for inner timber members $F_{v,0,Ed}$ is the accumulated load per fastener for the two shear planes

 $F_{ax,Rd}$ Minimum of the design values of the withdrawal capacity and the tensile capacity of the reinforcing full thread screws where I_{ef} is the smaller value of the penetration depth at the screw tip or head (see Fig. A.6.1)

If the timber under each fastener in a connection is reinforced, the effective number n_{ef} according to EN 1995-1-1, equation (8.34) may be taken as $n_{ef} = n$.



Figure A.6.1: Dowelled steel-to-timber connection with outer timber members and reinforcement;

Reinforcement of connections with laterally loaded dowel-type fasteners	
	Annex 6



ANNEX 7 Fastening of thermal insulation material on top of rafters

A.7.1 General

Würth screws with an outer thread diameter of at least 6 mm may be used for the fixing of thermal insulation material on top of rafters or on wood-based members in vertical façades. In the following, the meaning of the word rafter includes wood-based members with inclinations between 0° and 90°.

The thickness of the thermal insulation material may be up to 400 mm. The thermal insulation material shall be applicable as insulation on top of rafters or for façades according to national provisions that apply at the installation site.

The battens have to be from solid timber according to EN 338/EN 14081-1. The minimum thickness t and the minimum width b of the battens are given in Table A.7.1:

Outer thread diameter [mm]	Minimum thickness t [mm]	Minimum width b [mm]
6, 6.5, 7 and 8	30	50
10	40	60
12	80	100
14	100	100

Table A.7.1 Minimum thickness and minimum width of the battens

The minimum width of the rafters shall be 60 mm.

The spacing between screws shall be not more than 1.75 m.

Friction forces shall not be considered for the design of the characteristic axial load of the screws.

The anchorage of wind suction forces as well as the bending stresses of the battens shall be considered for design. Screws perpendicular to the grain of the rafter (angle $\alpha = 90^{\circ}$) may be arranged where required considering the design of the battens.

A.7.2 Parallel inclined screws and thermal insulation material in compression

A.7.2.1 Mechanical model

The system of rafter, thermal insulation material on top of rafter and counter battens parallel to the rafter may be considered as a beam on elastic foundation. The counter batten represents the beam, and the thermal insulation material on top of the rafter the elastic foundation. The minimum compressive stress of the thermal insulation material at 10 % deformation, measured according to EN 826¹, shall be $\sigma_{(10 \%)} = 0.05$ N/mm². The counter batten is loaded perpendicular to the axis by point loads F_b transferred by regularly spaced battens. Further point loads F_s are caused by the shear load of the roof due to dead and snow load, which are transferred from the screw heads into the counter battens.

Instead of battens the following wood-based panels may be used to cover the thermal insulation material if they are suitable for that use:

- Plywood according to EN 636 and EN 13986,
- Oriented Strand Board, OSB according to EN 300 and EN 13986,
- Particleboard according to EN 312 and EN 13986
- Fibreboards according to EN 622-2, EN 622-3 and EN 13986.

Only screws with countersunk head, 75 ° head, FBS head or woodwork head shall be used for fixing wood-based panels on rafters with thermal insulation material as interlayer.

The minimum thickness of the wood-based panels shall be 22 mm.

The word batten includes the meaning of the above mentioned wood-based panels in the following.

1	EN 826:2013	Thermal insulating products for building applications - Determination of compression beh	aviour

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Figure A.7.1 Fastening of the thermal insulation material on top of rafters - structural system

Würth self-tapping screws	
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Figure A.7.2 Point loads $F_{\rm b}$ perpendicular to the battens





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(7.2)

A.7.2.2 Design of the battens

It's assumed that the spacing between the counter battens exceeds the characteristic length I_{char} . The characteristic values of the bending stresses are calculated as:

$$M_{k} = \frac{(F_{b,k} + F_{s,k}) \cdot I_{char}}{4}$$

$$(7.1)$$

where

 $I_{char} = characteristic \ length \ I_{char} = 4 \sqrt{\frac{4 \cdot EI}{w_{ef} \cdot K}}$

EI = bending stiffness of the batten

K = coefficient of subgrade

 w_{ef} = effective width of the thermal insulation material

 $F_{b,k}$ = point loads perpendicular to the battens

 $\mathsf{F}_{s,k}$ = point loads perpendicular to the battens, load application in the area of the screw heads

The coefficient of subgrade K may be calculated from the modulus of elasticity E_{HI} and the thickness t_{HI} of the thermal insulation material if the effective width w_{ef} of the thermal insulation material under compression is known. Due to the load extension in the thermal insulation material the effective width w_{ef} is greater than the width of the batten or rafter, respectively. For further calculations, the effective width w_{ef} of the thermal insulation material may be determined according to:

where

w = minimum from width of the batten or rafter, respectively

t_{HI} = thickness of the thermal insulation material

$$\mathsf{K} = \frac{\mathsf{E}_{\mathsf{H}\mathsf{I}}}{\mathsf{t}_{\mathsf{H}\mathsf{I}}} \tag{7.4}$$

The following condition shall be satisfied:

$$\frac{\sigma_{m,d}}{f_{m,d}} = \frac{M_d}{W \cdot f_{m,d}} \le 1$$
(7.5)

For the calculation of the section modulus W the net cross section shall be considered.

The characteristic values of the shear stresses shall be calculated according to:

$$V_{k} = \frac{\left(F_{b,k} + F_{s,k}\right)}{2}$$

$$(7.6)$$

The following condition need to be satisfied:

$$\frac{\tau_{\rm d}}{f_{\rm v,d}} = \frac{1.5 \cdot V_{\rm d}}{A \cdot f_{\rm v,d}} \le 1 \tag{7.7}$$

For the calculation of the cross section area the net cross section shall be considered.

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A.7.2.3 Design of the thermal insulation material

The characteristic value of the compressive stresses in the thermal insulation material shall be calculated according to:

$$\sigma_{k} = \frac{1.5 \cdot F_{b,k} + F_{s,k}}{2 \cdot I_{char} \cdot w}$$
(7.8)

The design value of the compressive stress shall not be greater than 110 % of the compressive strength at 10 % deformation calculated according to EN 826.

A.7.2.4 Design of the screws

The screws are loaded predominantly axial. The characteristic value of the axial tension force in the screw may be calculated from the shear loads of the roof R_s :

$$T_{S,k} = \frac{R_{S,k}}{\cos\alpha}$$
(7.9)

The load-carrying capacity of axially loaded screws is the minimum design value of the axial withdrawal capacity of the threaded part of the screw, the head pull-through capacity of the screw and the tensile capacity of the screw according to Annex 2.

In order to limit the deformation of the screw head for thermal insulation material with thickness over 220 mm or with compressive strength below 0.12 N/mm², respectively, the axial withdrawal capacity of the screws shall be reduced by the factors k_1 and k_2 :

$$F_{ax,\alpha,Rd} = min \left\{ \frac{k_{ax} \cdot f_{ax,d} \cdot d \cdot l_{ef} \cdot k_1 \cdot k_2}{k_{\beta}} \cdot \left(\frac{\rho_k}{350} \right)^{0.8}; f_{head,d} \cdot d_h^2 \cdot \left(\frac{\rho_k}{350} \right)^{0.8}; \frac{f_{tens,k}}{\gamma_{M2}} \right\}$$
(7.10)

where:

- k_{ax} Factor according to Annex A.2.3.2, taking into account the angle α between screw axis and grain direction
- $f_{ax,d} $$ design value of the axial withdrawal parameter of the threaded part of the screw in the rafter $$ [N/mm^2] $$ N/mm^2]$

d outer thread diameter of the screw [mm]

- I_{ef} penetration length of the threaded part of the screw in the rafter [mm], $I_{ef} \ge 40$ mm
- ρ_k characteristic density of the wood-based member [kg/m³], for beech, ash and oak $\rho_k \le 590 \text{ kg/m}^3$ and for LVL (softwood) $\rho_k \le 500 \text{ kg/m}^3$

 α angle α between screw axis and grain direction, $30^{\circ} \le \alpha \le 90^{\circ}$

f_{head,d} design value of the head pull-through parameter of the screw [N/mm²]

d_h head diameter of the screw [mm]

f_{tens,k} characteristic tensile capacity of the screw according to Annex 2 [N]

 γ_{M2} partial factor according to EN 1993-1-1 in conjunction with the particular national annex

 k_1 min {1; 220/ t_{HI} }

k₂ min {1; $\sigma_{10\%}/0.12$ }

t_{HI} thickness of the thermal insulation material [mm]

 $\sigma_{10\%}$ compressive stress of the thermal insulation material under 10 % deformation [N/mm²]

 k_{β} Factor according to Annex A.2.3.2

If equation (7.10) is fulfilled, the deflection of the battens does not need to be considered when designing the loadcarrying capacity of the screws.

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A.7.3 Alternatively inclined screws and thermal insulation material non in compression

A.7.3.1 Mechanical model

Depending on the screw spacing and the arrangement of tensile and compressive screws with different inclinations the battens are loaded by significant bending moments. The bending moments are derived based on the following assumptions:

- The tensile and compressive loads in the screws are determined based on equilibrium conditions from the actions
 parallel and perpendicular to the roof plane. These actions are constant line loads q_⊥ and q_{||}.
- The screws act as hinged columns supported 10 mm within the batten or rafter, respectively. The effective column length consequently equals the length of the screw between batten and rafter plus 20 mm.

The batten is considered as a continuous beam with a constant span $\ell = A + B$. The compressive screws constitute the supports of the continuous beam while the tensile screws transfer concentrated loads perpendicular to the batten axis.

The screws are predominantly loaded in withdrawal or compression, respectively. The characteristic values of the screw's normal forces are determined based on the loads parallel and perpendicular to the roof plane:

Compressive screw:
$$N_{c,k} = (A + B) \cdot \left(-\frac{q_{II,k}}{\cos \alpha_1 + \sin \alpha_1 / \tan \alpha_2} - \frac{q_{\perp,k} \cdot \sin(90^\circ - \alpha_2)}{\sin(\alpha_1 + \alpha_2)} \right)$$
 (7.11)

Tensile screw:

$$+ (A + B) \cdot \left(\frac{q_{II,k}}{\cos \alpha_2 + \sin \alpha_2 / \tan \alpha_1} - \frac{q_{\perp,k} \cdot \sin(90^\circ - \alpha_1)}{\sin(\alpha_1 + \alpha_2)} \right)$$
(7.12)

A distance of the screws according to Figure A.7.5

 $N_{t,k} =$

B distance of the alternatively inclined screws according to Figure A.7.5

q_{II.k} characteristic value of the loads parallel to the roof plane

 $q_{\perp,k}$ characteristic value of the loads perpendicular to the roof plane

 α angle a_1 and a_2 between screw axis and grain direction, $30^\circ \le \alpha_1 \le 90^\circ$, $30^\circ \le \alpha_2 \le 90^\circ$

Only screws with full thread or a thread below the head and in the area of the drill tip shall be used.

The bending moments in the batten follow from the constant line load q_{\perp} and the load components perpendicular to the batten from the tensile screws. The span of the continuous beam is (A + B). The characteristic value of the load component perpendicular to the batten from the tensile screw is:

$$F_{ZS,k} = (A + B) \cdot \left(\frac{q_{II,k}}{1/\tan\alpha_1 + 1/\tan\alpha_2} - \frac{q_{\perp,k} \cdot \sin(90^\circ - \alpha_1) \cdot \sin\alpha_2}{\sin(\alpha_1 + \alpha_2)} \right)$$
(7.13)

A positive value for $F_{ZS,k}$ means a load towards the rafter, a negative value a load away from the rafter. The system of the continuous beam is shown in Figure A.7.5.

The battens or wood-based panels fixed on the rafter shall be supported perpendicular to the load-bearing plane.

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Figure A.7.4 Fastening of thermal insulation material on top of rafters - structural system for alternatively inclined screws



Figure A.7.5: Continuous batten under constant line loads from actions on the roof plane q_{\perp} and concentrated loads from tensile screws F_{ZS}

A.7.3.2 Design of the screws

The design value of the load-carrying capacity of the screws shall be calculated according to equations (7.14) and (7.15).

Screws loaded in tension:

$$\mathbf{F}_{\mathbf{ax},\alpha,\mathsf{Rd}} = \min\left\{\frac{\mathbf{k}_{\mathsf{ax}} \cdot \mathbf{f}_{\mathsf{ax},\mathsf{d}} \cdot \mathbf{d} \cdot \mathbf{I}_{\mathsf{ef},\mathsf{b}}}{\mathbf{k}_{\beta}} \cdot \left(\frac{\mathbf{p}_{\mathsf{b},\mathsf{k}}}{350}\right)^{0.8}; \frac{\mathbf{k}_{\mathsf{ax}} \cdot \mathbf{f}_{\mathsf{ax},\mathsf{d}} \cdot \mathbf{d} \cdot \mathbf{I}_{\mathsf{ef},\mathsf{r}}}{\mathbf{k}_{\beta}} \cdot \left(\frac{\mathbf{p}_{\mathsf{r},\mathsf{k}}}{350}\right)^{0.8}; \frac{\mathbf{f}_{\mathsf{tens},\mathsf{k}}}{\gamma_{\mathsf{M2}}}\right\}$$
(7.14)

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Screws loaded in compression:

$$F_{ax,\alpha,Rd} = \min\left\{\frac{k_{ax} \cdot f_{ax,d} \cdot d \cdot l_{ef,b}}{k_{\beta}} \cdot \left(\frac{\rho_{b,k}}{350}\right)^{0.8}; \frac{k_{ax} \cdot f_{ax,d} \cdot d \cdot l_{ef,r}}{k_{\beta}} \cdot \left(\frac{\rho_{r,k}}{350}\right)^{0.8}; \frac{\kappa_{c} \cdot N_{pl,k}}{\gamma_{M1}}\right\}$$
(7.15)

where:

k _{ax}	Factor according to Annex A.2.3.2, taking into account the angle α between screw axis and grain direction
f _{ax,d}	design value of the axial withdrawal capacity of the threaded part of the screw [N/mm ²]
d	outer thread diameter of the screw [mm]
I _{ef,b}	penetration length of the threaded part of the screw in the batten [mm]
I _{ef,r}	penetration length of the threaded part of the screw in the rafter, $I_{ef} \ge 40 \text{ mm}$
k_{β}	Factor according to Annex A.2.3.2
$\rho_{b,k}$	characteristic density of the batten [kg/m ³], for beech, ash and oak $\rho_k \le 590$ kg/m ³ and for LVL (softwood) $\rho_k \le 500$ kg/m ³
$\rho_{\textbf{r},\textbf{k}}$	characteristic density of the rafter [kg/m ³], for beech, ash and oak $\rho_k \le 590$ kg/m ³ and for LVL (softwood) $\rho_k \le 500$ kg/m ³
α	angle α_1 or α_2 between screw axis and grain direction, $30^\circ \le \alpha_1 \le 90^\circ$, $30^\circ \le \alpha_2 \le 90^\circ$
f _{tens,k}	characteristic tensile capacity of the screw according to Annex 2 [N]
γм1, γм2	partial factor according to EN 1993-1-1 in conjunction with the particular national Annex
$\kappa_{c}\cdotN_{pl,k}$	Buckling capacity of the screw according to table A.7.2 [N]

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Free screw			ASSY plus	s VG		ASSY Isotop
length l between	Outer thread diameter d [mm]					
batten and	6.0	8.0	10.0	12.0	14.0	8.0/ 10.0
rafter [mm]	κ _c · N _{pl,k} [kN]					
≤ 100	1.12	3.26	8.24	13.30	21.8	10.1
120	0.85	2.48	6.37	10.40	17.4	8.30
140	0.66	1.95	5.06	8.32	14.1	6.84
160	0.53	1.57	4.10	6.78	11.6	5.70
180	0.43	1.17	3.39	5.63	9.61	4.79
200	-	1.08	2.86	4.74	8.14	4.08
220	-	0.91	2.43	4.05	6.96	3.51
240	-	0.78	2.09	3.50	6.03	3.04
260	-	0.68	1.81	3.05	5.25	2.67
280	-	0.59	1.60	2.68	4.65	2.35
300	-	0.53	1.40	2.37	4.11	2.10
320	-	0.47	1.25	2.10	3.67	1.88
340	-	0.42	1.12	1.90	3.30	1.69
360	-	0.37	1.01	1.71	2.98	1.53
380	-	0.34	0.92	1.55	2.70	1.45
400	-	0.31	0.83	1.42	2.46	1.26
420	-	0.28	0.77	1.30	2.25	1.16
440	-	0.26	0.70	1.18	2.06	1.06
460	-	0.24	0.65	1.10	1.91	0.99
480	-	0.22	0.59	1.01	1.77	0.91

Table A.7.2 Characteristic load-carrying capacity of the screws $\kappa_c \cdot N_{pl,k}$ in kM	carrying capacity of the screws $\kappa_{c} \cdot N_{pl,k}$ in kN
---	---

Würth self-tapping screws

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ANNEX 8 Effective number of screws n_{ef} arranged under an angle $30^{\circ} \le \alpha \le 60^{\circ}$ between the shear plane and the screw axis

Alternatively to clause A.2.3.2, the load-carrying capacity may be calculated using the effective number of fasteners n_{ef} for one row of n inclined screws or crossed screw couples in timber-to-timber or steel-to-timber single shear connections parallel to the load, where the screws are arranged under an angle $30^{\circ} \le \alpha \le 60^{\circ}$ between the shear plane and the screw axis:

$$\mathbf{n}_{\rm ef} = \frac{1}{\max\left(\delta_1; \delta_2\right)} \tag{8.1}$$

Where:

$$\delta_1 = 1 - m_1 \cdot (1 + \mu) + \mu + \frac{m_1 - m_2}{m_1^n - m_2^n} \cdot (m_1^n \cdot (1 + \mu) - \mu)$$
(8.2)

$$\delta_2 = -\mu + m_1^{n-1} \cdot (1+\mu) - \frac{m_1^{n-1} - m_2^{n-1}}{m_1^n - m_2^n} \cdot (m_1^n \cdot (1+\mu) - \mu)$$
(8.3)

$$\mu = -\frac{1}{1 + \frac{E_1 A_1}{E_2 A_2}}$$
(8.4)

E₁A₁ Axial stiffness of side member 1

 E_2A_2 Axial stiffness of side or middle member 2. If member 2 is a middle member, A_2 is only half of the member cross-section

 E_1, E_2 Mean value of modulus of elasticity of member 1 and member 2

A₁, A₂ Cross-sectional area of member 1 and member 2

- K_u Slip modulus parallel to the shear plane per screw (inclined screws) or per screw couple (crossed screws) for the ultimate limit state
- n Number of inclined screws or crossed screw couples per row
- m Number of rows of inclined screws or crossed screw couples per shear plane

$$m_{1} = 0.5 \cdot \left(\omega + \sqrt{\omega^{2} - 4}\right)$$

$$m_{1} = 0.5 \cdot \left(\omega - \sqrt{\omega^{2} - 4}\right)$$
(8.5)
(8.6)

$$\omega = 2 + K_u \cdot a_1 \left(\frac{m}{E_1 A_1} + \frac{m}{E_2 A_2} \right)$$
(8.7)

a₁ Screw spacing parallel to grain

Würth self-tapping screws	A
Effective number of screws n _{ef}	Annex 8



1) ASSY, AMO, JAMO (all kinds without ASSY plus VG and Isotop)



Full thread without drilling tip



Partial thread without drilling tip



Full thread with drilling tip



Partial thread with drilling

All ASSY, AMO and JAMO screws can be like on the drawing (I) or without thread in the middle of screw (II) or without thread below head (III) or in combination (IV). The thread can be manufactured to customer specific within 4 x d and Ig max.



Possible surface coatings: blank; brass-plated; nickel-plated; browned; zinc plated; zinc plated blue passivated, yellow chromated, black chromated; zinc-nickel plated, zinc-nickel plated passivated; zinc flakes; ruspert; completly or partially painted, hot tip galvanized; aluminium coating; phosphated; HCP coated, delta coated - surface coatings can be combined together. The minimum thickness of the zinc coating of the screws is 5 μ m and of the zinc-nickel coating 4 μ m.

WÜRTH self-tapping screws

Drawings of ASSY, JAMO and AMO screws

















Lengths for d = 3.0 mm, stainless steel

lg
+1.0
-2.0
12
49

Screws without thread in the middle of screw or without thread below head or in combination of both are possible (see Annex 9.1). The thread lengths can be manufactured to costumer specific within Ig min and Ig max.

All dimensions in mm.

WÜRTH self-tapping screws

ASSY, ASSY plus, Jamo, Jamo plus - d = 3.0 mm and d = 3.4 mm, stainless steel























Rings on the shank for d = 3.5 mm, carbon steel



Rings on the shank can also be formed as a thread. Rings or thread with the same shape can be all over the shank or only on parts of it.

All dimensions in mm.

Lengths for d = 3.5 mm, carbon steel

1	lg
+1.0	+1.0
-2.0	-2.0
16	14
50	48

Screws without thread in the middle of screw or without thread below head or in combination of both are possible (see Annex 9.1). The thread lengths can be manufactured to costumer specific within Ig min and Ig max.

All dimensions in mm.

WÜRTH self-tapping screws

ASSY, ASSY plus, Jamo, Jamo plus - d = 3.5 mm and d = 3.9 mm, carbon steel













WÜRTH self-tapping screws

ASSY, ASSY plus, Jamo, Jamo plus - d = 3.5 mm and d = 3.9 mm















Rings on the shank for d = 4.0 mm, carbon steel



Rings on the shank can also be formed as a thread. Rings or thread with the same shape can be all over the shank or only on parts of it.

All dimensions in mm.

Lengths for d = 4.0 mm, carbon steel

l +1.0 -2.0	lg +1.0 -2.0
18	16
70	68

Screws without thread in the middle of screw or without thread below head or in combination of both are possible (see Annex 9.1). The thread lengths can be manufactured to costumer specific within Ig min and Ig max.

All dimensions in mm.

WÜRTH self-tapping screws

ASSY, ASSY plus, Jamo, Jamo plus - d = 4.0 mm and d = 4.4 mm, carbon steel













Rings on the shank for d = 4,4 mm, all materials



Rings on the shank can also be formed as a thread. Rings or thread with the same shape can be all over the shank or only on parts of it.

All dimensions in mm.

Lengths for d = 4.4 mm, all materials

1	lg
+1.0	+1.0
-2.0	-2.0
16	14
80	66

Screws without thread in the middle of screw or without thread below head or in combination of both are possible (see Annex 9.1). The thread lengths can be manufactured to costumer specific within Ig min and Ig max.

All dimensions in mm.

WÜRTH self-tapping screws

ASSY, ASSY plus, Jamo, Jamo plus - d = 4.0 mm and d = 4.4 mm















Rings on the shank for d = 4.5 mm, carbon steel



Rings on the shank can also be formed as a thread. Rings or thread with the same shape can be all over the shank or only on parts of it.

All dimensions in mm.

Lengths for d = 4.5 mm, carbon steel

1	lg
+1.0	+1.0
-2.0	-2.0
20	18
100	78

Screws without thread in the middle of screw or without thread below head or in combination of both are possible (see Annex 9.1). The thread lengths can be manufactured to costumer specific within Ig min and Ig max.

All dimensions in mm.

WÜRTH self-tapping screws

ASSY, ASSY plus, Jamo, Jamo plus - d = 4.5 mm, carbon steel











Head types for d = 5.0 mm and d = 5.5 mm, all materials



Countersunk head design with and without raise, with and without milling pockets



Countersunk head with cutter ribs design with and without raise

Ø**9,0** ±0,45

Pan Head

Large washer head I

Ø12,0 ±0,5

က်

3,0 ±0,3



Countersunk head design with and without raise, with and without milling pockets



Countersunk head with cutter ribs design with and without raise

Ø**10,0** ±0,5

Pan Head

Large washer head II -

design with and without

cutter ribs

Ø11,0 ±0,6

3.6 ±0.

03



Countersunk head design with and without raise, with and without milling pockets



Countersunk head with cutter ribs design with and without raise

Ø 12,0 ±0,5

Pan Head

Large washer head III -

design with and without

cutter ribs

Ø10 ±0,5

å

0 4

±0.3

2



Countersunk head design with and without raise, with and without milling pockets



Countersunk head with cutter ribs design with and without raise



Step Head

2.8±0,3



Large washer head III design with and without cutter ribs

WÜRTH self-tapping screws

±0,5

ø Ñ

ASSY, ASSY plus, Jamo, Jamo plus - d = 5.0 mm and d = 5.5 mm

 \emptyset **8,9** ±0,5











Rings on the shank for thread types d = 5.0 mm, carbon steel



Rings on the shank can also be formed as a thread. Rings or thread with the same shape can be all over the shank or only on parts of it.

All dimensions in mm.

Lengths for d = 5.0 mm, carbon steel

1	lg	Shank cutter	Shank cutter at plus/	Shank cutter
+1.0	+1.0	at partial	plus 3.0/ plus special	
-2.5	-2.0	thread	partial thread	
22	20	up to L = 90:	over all lengths optional	
		optional		$ \begin{array}{c} & & & \\ & & & & \\ & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & $
		over L = 90		
		yes		
120	90			$04,2\pm0,4$

Screws without thread in the middle of screw or without thread below head or in combination of both are possible (see Annex 9.1). The thread lengths can be manufactured to costumer specific within Ig min and Ig max.

All dimensions in mm.

WÜRTH self-tapping screws

ASSY, ASSY plus, Jamo, Jamo plus - d = 5.0 mm and d = 5.5 mm, carbon steel












Head types for d = 6.0 mm, d = 6.3 mm and d = 6.5 mm, all materials



Hexalobular head – design with and without collar



Alternatively at countersunk heads: modification of the shank at drilled head I



Jamo head I



Underhead thread Lg2 < 4 x d, P= 2.6, 3.6, 5.2



Hexalobular head – design with and without collar



Elmo head



Jamo head II – design with and without milling pockets



Underhead thread Lg2 < 4 x d, P= 2.6



Kombi hexagonal head



Truss head – design with and without cutter ribs or flange



Stud head Design with and without hexagonal part



Hexagonal head with and without collar



Cylinder head



Underhead thread – Type P

WÜRTH self-tapping screws

ASSY, ASSY plus, Jamo, Jamo plus - d = 6.0 mm, d = 6.3 mm and d = 6.5 mm











Thread types d = 6.3 mm, all materials



Lengths for d = 6.3 mm, all materials

lg
+1.0
-2.0
25,2
60

Screws without thread in the middle of screw or without thread below head or in combination of both are possible (see Annex 9.1). The thread lengths can be manufactured to costumer specific within Ig min and Ig max.

All dimensions in mm.

WÜRTH self-tapping screws

ASSY WG-Fix d = 6.3 mm





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Lengths for d = 8.0 mm, stainless steel, for above threads

l +1.0 -5.0	lg +1.0 -2.5	Shank cutter at partial thread	Shank cutters
35	32	up to I = 150: optional	
		over I = 150: yes	
400	160		

Screws without thread in the middle of screw or without thread below head or in combination of both are possible (see Annex 9.1). The thread lengths can be manufactured to costumer specific within Ig min and Ig max. All dimensions in mm.

WÜRTH self-tapping screws

ASSY, ASSY plus, Jamo, Jamo plus - d = 7.5 mm and 8.0 mm









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1	Ig	Shank cutter at partial thread	Shank cutters		
+1.0	+1.0		Ø 8,6 ±0,3	0,0	
-5.0	-2.5			10,5	Ø7,9 ±0,5
45	40	up to I = 150: optional	0'5	1 AM	-50,010,010,010
		over I = 150: yes		Ø8.0 ±0.5	
400	200			\$0,010,0	1

Screws without thread in the middle of screw or without thread below head or in combination of both are possible (see Annex 9.1). The thread lengths can be manufactured to costumer specific within Ig min and Ig max.

All dimensions in mm.

WÜRTH self-tapping screws

ASSY, ASSY plus, Jamo, Jamo plus - d = 10.0 mm, stainless steel





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WÜRTH self-tapping screws

ASSY, ASSY plus, Jamo, Jamo plus - d = 12.0 mm, carbon steel



Head types for ASSY plus VG d = 6.0 mm, carbon steel



Countersunk head – design with and without raise, with and without milling pockets



Cylinder head

Ø14,0 ±0,5



Countersunk head – design with and without raise, with and without milling pockets





Hexalobular head with and without collar



Countersunk head – design with and without raise, with and without milling pockets



Hexalobular head with and without collar



Ø**12** ±0,5

Countersunk head with cutter ribs – design with and without raise



Kombi hexagonal head with and without collar



Truss head – design with and without cutter ribs or flange



Large washer head III – design with and without cutter ribs



Large washer head II

Large washer head I

a max









Head types for ASSY plus VG d = 8.0 mm, carbon steel

±0,4

ŝ



Countersunk head – design with and without raise, with and without milling pockets



Countersunk head – design with and without raise, with and without milling pockets



Large washer head III – design with and without cutter ribs



Hexalobular head



Countersunk head – design with and without raise, with and without milling pockets



Countersunk head with cutter ribs – design with and without raise



Large washer head III – design with and without cutter ribs



Hexalobular head



Countersunk head – design with and without raise, with and without milling pockets



Large washer head I



Large washer head III – design with and without cutter ribs



Cylinder head



Countersunk head – design with and without raise, with and without milling pockets



Large washer head II – design with and without cutter ribs



Truss head – design with and without cutter ribs or flange



Kombi hexagonal head with and without collar





Head types for ASSY plus VG d = 8.0 mm, carbon steel



Stud head Design with and without hexagonal part

WÜRTH self-tapping screws

ASSY plus VG screws, carbon steel -d = 8 mm







Head types for ASSY plus VG d = 10.0 mm, carbon steel



Countersunk head – design with and without raise, with and without milling pockets



Countersunk head with cutter ribs – design with and without raise



Cylinder head



Large washer head I

WÜRTH self-tapping screws

ASSY plus VG screws, carbon steel - d = 10 mm



Countersunk head – design with and without raise, with and without milling pockets



Kombi hexagonal head with and without collar



Hexalobular head with and without collar



Large washer head II – design with and without cutter ribs



Countersunk head – design with and without raise, with and without milling pockets



Kombi hexagonal head with and without collar



Hexalobular head with and without collar



Large washer head III – design with and without cutter ribs



Countersunk head – design with and without raise, with and without milling pockets



Stud head Design with and without hexagonal part



Truss head – design with and without cutter ribs or flange



Large washer head III – design with and without cutter ribs

Annex 9.62







Head types for ASSY plus VG d = 12.0 mm, carbon steel



Countersunk head – design with and without raise, with and without milling pockets



Cylinder head



Large washer head III – design with and without cutter ribs



Countersunk head – design with and without raise, with and without milling pockets



Hexalobular head with or without collar



Large washer head I



Countersunk head – design with and without raise, with and without milling pockets



Hexalobular head with or without collar



Truss head – design with and without cutter ribs or flange



Countersunk head – design with and without raise, with and without milling pockets



Kombi hexagonal head with and without collar

ASSY plus VG screws, carbon steel - d = 12 mm











nread	types AS		$\mathbf{\hat{S}} d = 14.0 \text{ mm, c}$	arbon steel	Schnitt A-	A
esign v	vith and withc	out cutting ed	ges (see section (Sc	hnitt) A-A), Design o	of drilling tip c	an be according to plue
ength	s for ASS	Y plus VG	d = 14.0 mm, ca	rbon steel		
	Counte	ersunk and C	ylinder head	Large	washer-, Hex Hexalobular	•
	l +1.0	lg +5.0	a max	l +1.0	lg +10.0	a max
	-5.0 120	-12.0 105	22.0	-5.0 120	-7.0 105	17.0
	200	185	22.0	200	185	17.0
	l +10.0 -20.0	lg +14.0 -32.0	a max	l +5.0 -15.0	lg +14.0 -22.0	a max
	210	195	27.0	210	195	22.0
	 800	 785	27.0	 800	 785	22.0
	l +10.0 -20.0	lg +14.0 -32.0	a max	 +10.0 -20.0	lg +19.0 -27.0	a max
	810	795	27.0	810	795	22.0
	2000	1985	27.0	2000	1985	22.0
Part wi All dim	thout thread ensions in mi	below head/ (ee Annex 9.1): Part Combination of both. Axd.		e middle of so	rew/
	self-tapping s	screws				
ÜRTH	son tapping s					









WÜRTH self-tapping screws

Head marking



Countersunk washers pressed, material steel, aluminum and stainless steel



Dimensions (all dimensions in mm):

Size	t ±0.4	D ±0.5	d +0.5	h +0.5	Ds ±1	s ±0.75
6	2.5	22	6.5	3.0	13.0	2.4
8	3.0	28	8.5	3.5	16.0	3.3
10	3.0	33	10.5	4.3	19.5	3.4
12	4.0	42	12.5	5.0	23.0	3.0

Countersunk washers turned, material steel, aluminum and stainless steel



Dimensions steel and aluminum (all dimensions in mm):

Size	d ±0.2	D ±0.5	h +0.3	al (°)	d2 ±0.3	d3 ±0.3
6	6.4	22.0	4.5	45	14.0	15.0
8	8.4	25.0	5.0	41	17.0	18.0
10	10.4	30.0	7.0	37	20.0	21.0
12	12.4	40.0	8.5	47	23.0	24.0

Dimensions stainless steel (all dimensions in mm):

Size	d1 ±0.2	D ±0.5	h +0.3	al (°)	d2 ±0.3	d3 ±0.3
6	6.4	22.0	3.8	45	14.0	14.5
8	8.4	25.0	5.0	45	18.4	19.0
10	10.4	30.0	7.0	37	20.0	21.0

WÜRTH self-tapping screws

Washers



Washers for large washer head II, material steel and stainless steel, turned



Dimensions (all dimensions in mm):

Size	d +0.4	D ±0.5	h ±0.3	s ±0.2	ds +0.5	RA ±0.1	W ±3°
5	9	15	3,5	1,0	11,7	2	150
6	11	22	5	1,1	14,5	3	150
7	12	25	5,5	1,4	16,2	3	150
8	12	30	6,5	1,4	19,0	4	150
12	17	42	8,5	1,9	27,5	5	150

Countersunk washers 45°, material steel and stainless steel, turned, used in wood-wood constructions





Dimensions (all dimensions in mm):

Size	d ±0.3	D ±0.5	Ds ±0.3	h ±0.5	L ±0.5	n ±0.5
8	8.5	25	15.9	14	18.2	12.9

WÜRTH self-tapping screws	
Washers	Annex 9.71



Countersunk washers 45°, material steel cast and stainless steel cast





Dimensions (all dimensions in mm):

Size	d	D	L	а	h	h1	b	1	k	n
	±0.3	±0.5	±1	±0.5	±0.8	±0.4	±0.2	±0.3	±0.3	±0.5
6	6.5	14.5	20.5	17.0	13.5	2.7	6.9	22.7	13.5	10.7
8	8.5	19.0	39.0	24.0	16.0	3.7	9.9	31.7	21.0	12.7
10	10.7	24.0	52.0	29.0	21.4	4.7	10.8	43.7	28.7	18.4
12	12.7	26.0	59.0	30.0	23.5	5.6	12.8	49.7	34.0	19.8

Countersunk washers 45°, material carbon steel and stainless steel, turned, used in steelwood constructions



Dimensions (all dimensions in mm):

Size	d ±0.3	D ±0.5	d1 ±0.2	d2 ±0.5	h ±0.8	h1 ±0.3	n ±0.5	R-Sphere ±0.5
6	6.5	12	12.9	20.0	10.0	1.9	8.0	10
8	8.5	15	15.9	25.0	11.6	1.9	9.5	12.5

Washers: Galvanized steel and stainless steel material according to DIN 436, DIN 440, EN 7093 and EN 9021 with the following possible surface coatings: blank; brass-plated; nickel-plated; browned; zinc plated; zinc plated blue passivated, yellow chromated, black chromated; zinc-nickel plated, zinc-nickel plated passivated; zinc flakes; ruspert; HCP, completly or partially painted, hot tip galvanized; aluminium coating phosphated; delta coated - surface coatings can be combined

WÜRTH self-tapping screws

Washers



Washer for tinner screws, material 1: stainless steel or copper, material 2: EPDM sealent (is not part of the ETA)



Dimensions (all dimensions in mm)

Size	øA1	øA2	øD1	øD2	T1	T2	Т3
15	15 ±0.50	14 ±0.6	5.4 ±0.6	3.0 ±0.5	3.0 ±0.6	0.5 ±0.2	1.9 ±0.5
20	20 ±0.50	19 ±0.6	5.4 ±0.6	3.0 ±0.5	3.4 ±0.6	0.5 ±0.2	1.9 ± 0.5
25	25 ±0.50	24 ±0.6	5.4 ±0.6	3.0 ± 0.5	3.8 ±0.6	0.5 ±0.2	1.9 ± 0.5

WÜRTH self-tapping screws

Washers